

# Spectral encapsulation of OFDM systems based on orthogonalization for short packet transmission

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## Funding information

This work was supported by the Agency for Defense Development, Republic of Korea under Grant UD170022DD.

A spectrally encapsulated (SE) orthogonal frequency-division multiplexing (OFDM) precoding scheme for wireless short packet transmission, which can suppress the out-of-band emission (OoBE) while maintaining the advantage of the cyclic prefix (CP)-OFDM, is proposed. The SE-OFDM symbol consists of a prefix, an inverse fast Fourier transform (IFFT) symbol, and a suffix generated by the head, center, and tail matrices, respectively. The prefix and suffix play the roles of a guard interval and suppress the OoBE, and the IFFT symbol has the same size as the discrete Fourier transform symbol in the CP-OFDM symbol and serves as an information field. Specifically, as the center matrix generating the IFFT symbol is orthogonal, data and pilot symbols can be allocated to any subcarrier without distinction. Even if the proposed precoder is required to generate OFDM symbols with spectral efficiency in the transmitter, a corresponding decoder is not required in the receiver. The proposed scheme is compared with CP-OFDM in terms of spectrum, OoBE, and bit-error rate.

## KEYWORDS

filter, matrix, OFDM, orthogonal, out-of-band, precoder, prefix, spectrum, suffix

## 1 | INTRODUCTION

The orthogonal frequency-division multiplexing (OFDM) transmission scheme has a distinct advantage in that transmission can be made secure by effectively estimating and correcting a multipath channel. However, as the envelope function is a square wave [1], the spectrum is spread and the out-of-band power is leaked to adjacent channels [2].

Windowing in the time domain has been studied to suppress spectral sidelobes [3]. However, a guard interval is added to the OFDM symbol to smooth the transition between consecutive symbols, thereby reducing transmission throughput. The general restraints on the spectral precoding of zero-padding-OFDM and cyclic prefix (CP)-OFDM have been discovered, and block-division CP-OFDM, which

facilitates the design of a precoder with spectral efficiency, has been proposed based on these techniques [4]. In addition, a technique has been proposed that includes a no-guard-OFDM scheme with no guard interval inserted. This is then combined with a spectrally compact precoder, as it avoids spreading of the spectrum [5]. To improve spectral efficiency, pilot patterns were designed to optimize the channel estimation of multipath channels and suppress spectral sidelobes in a system that processes data and pilot waveforms individually to provide spectral compactness [6]. It is necessary to create subcarriers for transmitting the pilot symbols separately from the subcarriers that transmit the data symbols because the pilot subcarrier and data subcarrier may have many common frequency components. Emission suppression was first treated as a problem of minimizing

the Frobenius norm of the matrix, and then an orthogonal precoding scheme was developed based on singular value decomposition (SVD) to obtain significant performance [7]. To eliminate the discontinuity between consecutive OFDM symbols, the relationship between the previous symbol and the current symbol was derived in the form of a matrix equation through the  $N$ -th differentiation, and a method of reducing the out-of-band emission (OoBE) by updating the data vector and specific gravity vector was proposed [8]. As this method has a cyclic structure and a concatenation error may occur, it is disadvantageous in that it cannot be applied to the burst mode communication method. To reduce jointly the OoBE and peak-to-average power ratio of the OFDM-based system, a method called alignment suppression, which generates a suppression signal, has been proposed [9]. As this method utilizes the original redundant CP in the OFDM symbol, it does not reduce transmission efficiency. It is also possible to perform demodulation similar to legacy OFDM without changing the receiver structure. However, as the transmitter uses the channel state information (CSI), a secure channel is required in the reverse direction, and the receiver has complexity in calculation for the extraction of CSI from the received signal. In addition, the suppression signal may be leaked to the data owing to the incomplete channel information, and there may be a deterioration of the bit-error rate (BER) performance and a decrease in the synchronization performance owing to the change in the CP. In filter bank multicarrier (FBMC) which is a filtered multi-carrier system, subcarriers are individually shaped to reduce OoBE [10]. Usually, as the subcarriers have a length of four times the symbol length, this method is not suitable for the future requirements of high transmission efficiency with short delay. A multicarrier modulation scheme called generalized frequency-division multiplexing (GFDM) has been proposed [11], which includes the case of CP-OFDM and single-carrier frequency-domain equalization. However, with the exception of these special cases, subcarrier filtering results in non-orthogonality between subcarriers. Consequently, intersymbol interference (ISI) and intercarrier interference occur, and hence, to eliminate them, the complexity of the receiver increases. A filtered (F)-OFDM scheme that limits OoBE by filtering OFDM symbols has been proposed [12]. However, when applied to short-length OFDM symbols, the F-OFDM scheme results in ISI/interchannel interference (ICI) and can affect synchronization and BER performance because it allows the length of the filter to be half the length of the OFDM symbol. A scheme has been proposed in which a transmitter reduces OoBE by combining existing OFDM and cancellation carriers, and a receiver can perform demodulation in the same manner as an existing OFDM demodulation scheme [13]. This approach generalized and unified existing active interference cancellation and time-domain OoBE suppression schemes.

This method was also shown to satisfy the spectral mask specified in the EN-50560 standard. The method greatly improved the spectral characteristics compared with the previous methods [14–16]. Compared with the raised cosine pulse method, the proposed method improves the data carrier loss from 28% to <4%.

In this study, we propose a precoding scheme that maintains the merits of CP-OFDM and can solve the problem of OoBE. The proposed scheme provides high blocking characteristics by forming spectral nulls at the upper and lower boundaries of the signal band. Numerous existing schemes, such as channel and frequency offset estimations in CP-OFDM, can be applied to the proposed scheme. As the proposed precoding scheme has no effect on the inverse fast Fourier transform (IFFT) symbol and is compatible with the legacy OFDM scheme, the pilot symbol can be transmitted without any sacrifice. Therefore, the proposed scheme has no self-interference between subcarriers and has the same BER performance as CP-OFDM.

The rest of this paper is organized as follows. Section 2 describes the baseband communication model with the proposed precoding scheme to develop and verify the proposed scheme. Section 3 describes the precoder matrix generation process and the approximation of the generated precoder. The pilot insertion scheme is considered in the proposed scheme. Section 4 provides an example of precoder matrix generation with the short OFDM symbol defined in IEEE 802.11a [17] and the precoding structure defined in IEEE 802.11g [18], and analyzes its frequency response characteristic. In Section 5, the BER performance of the proposed scheme in additive white Gaussian noise (AWGN) and multipath fading channel environments is measured and compared with that of CP-OFDM. Section 6 summarizes the results of this study and suggests applicable communication fields.

## 2 | COMMUNICATION MODEL

The communication system model using the proposed precoding scheme is shown in Figure 1. The data source generates binary data and is mapped to a quadrature amplitude modulation (QAM) symbol using a symbol mapper. Through the pilot insertion block, the pilot symbols can be transmitted at locations based on a predetermined rule. The precoder converts an input vector into an OFDM symbol, which consists of a prefix, an IFFT symbol, and a suffix. The P/S converter converts the parallel OFDM symbol to the serial sample sequence. The channel is modeled as an AWGN and multipath fading channel. The Select IFFT symbol selects the IFFT symbol in the received OFDM symbol. The S/P converts the serial sample sequence into a parallel vector. The FFT transforms the input vector from

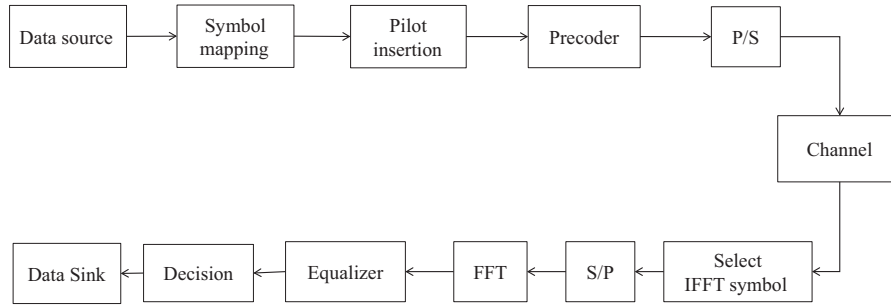


FIGURE 1 Communication system model

the time domain to the frequency domain. The equalizer block can extract the pilot symbols and perform equalization. The decision block decides the input samples as QAM symbols, converts them into binary data, and sends them to the sink block. As in CP-OFDM, the feature of this model is that there is no decoder in the receiver corresponding to the precoder in the transmitter because the IFFT symbol carrying the data symbols is not changed by the precoder.

### 3 | PRECODER MATRIX GENERATION PROCESS

The process of generating a precoder through six functional blocks is shown in Figure 2. The precoder matrix is generated by using the carrier matrix used in CP-OFDM as a mapping matrix, converting the matrix into the time domain, adding a prefix and suffix, weighting, zero insertion, and orthogonalization. The orthogonalization involves orthogonalizing the matrix such that the subcarriers transmitting the data symbols are orthogonal to one another. Similar to CP-OFDM, the precoder performs almost the same function as converting the input data symbol to the time domain through the inverse discrete Fourier transform (IDFT).

#### 3.1 | Mapping matrix J

The arrangement of the OFDM subcarriers in the frequency domain can be represented by the following general matrix:

$$\mathbf{J} (\in \mathbb{R}^{N \times M}) = \begin{bmatrix} \mathbf{0}_{dc} & & & & \\ & \mathbf{I}^+ & & & \\ & & & & \\ & & & \mathbf{0}_g & \\ & & & & \mathbf{I}^- \end{bmatrix}, \quad (1)$$

where  $N$  and  $M$  are the FFT size and the number of data symbols, respectively [19,20]. The zero matrices are the direct current (DC) subcarrier

$$\mathbf{0}_{dc} = \mathbf{0}^{(1 \times \frac{M}{2})}, \quad (2)$$

the positive and negative identity matrices

$$\mathbf{I}^+ = \mathbf{I}^- = \mathbf{I}_{\frac{M}{2}} = \text{diag} \left( \left[ \overbrace{1, 1, \dots, 1}^{M/2} \right] \right), \quad (3)$$

and the zero guard matrix.

$$\mathbf{0}_g = \mathbf{0}^{(\beta \times \frac{M}{2})}, \quad (4)$$

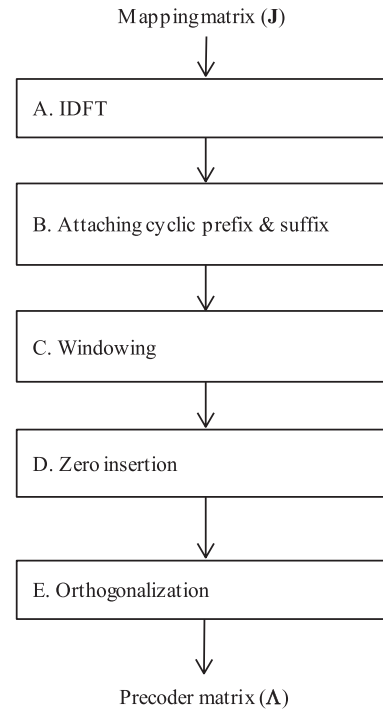


FIGURE 2 Precoder generation process

and all spaces are zero. When the parameter  $\beta = 0$ , there is no guard subcarrier.

### 3.2 | Transformation of the mapping matrix to the time domain

Each column of the mapping matrix can be converted from the frequency domain to the time domain by obtaining the  $N$ -point IDFT as.

$$\mathbf{P} = \mathbf{F}_N^H \mathbf{J}, \quad (5)$$

where  $\mathbf{P} \in \mathbb{C}^{N \times M}$  and  $\mathbf{F}_N \in \mathbb{C}^{N \times M}$  is the discrete Fourier transform (DFT) matrix

$$\mathbf{F}_N = \frac{1}{\sqrt{N}} \left[ e^{-j \frac{2\pi mn}{N}} \right]_{-N/2 \leq m, n \leq N/2-1}. \quad (6)$$

As the matrix  $\mathbf{P}$  is orthogonal, it can be expressed using a matrix  $\mathbf{A} \in \mathbb{C}^{N \times M}$  as

$$\mathbf{P} = \mathbf{A} (\mathbf{A}^H \mathbf{A})^{-\frac{1}{2}}. \quad (7)$$

The matrix  $\mathbf{A}$  can be decomposed by SVD as

$$\mathbf{A} = \mathbf{U} \mathbf{\Sigma} \mathbf{V}^H, \quad (8)$$

where  $\mathbf{U}$  and  $\mathbf{V}$  are unitary matrices and  $\mathbf{\Sigma} = \begin{bmatrix} \mathbf{S} \\ \mathbf{0} \end{bmatrix}$ . The matrix

$$\mathbf{S} = \text{diag}(s_1 \ s_2 \ \dots \ s_M) \quad (9)$$

is a diagonal matrix with eigenvalues and  $\mathbf{0} \in \mathbb{R}^{(N-M) \times M}$  is a zero matrix. From Appendix A, we have

$$\begin{aligned} \mathbf{P} &= \mathbf{U} \mathbf{\Sigma} \mathbf{V}^H \left( (\mathbf{U} \mathbf{\Sigma} \mathbf{V}^H)^H (\mathbf{U} \mathbf{\Sigma} \mathbf{V}^H) \right)^{-\frac{1}{2}} \\ &= \mathbf{U} \begin{bmatrix} \mathbf{I}_M \\ \mathbf{0} \end{bmatrix} \mathbf{V}^H \\ &= \mathbf{U} \mathbf{K} \mathbf{V}^H, \end{aligned} \quad (10)$$

where  $\mathbf{K} \in \mathbb{R}^{(N \times M)} = \begin{bmatrix} \mathbf{I}_M \\ \mathbf{0} \end{bmatrix}$ . This result indicates that  $\mathbf{P}$  can be represented by the product of two unitary matrices and an identity matrix, and the orthogonality can be verified by  $\mathbf{P}^H \mathbf{P} = \mathbf{V} \mathbf{K}^H \mathbf{U}^H \mathbf{U} \mathbf{K} \mathbf{V}^H = \mathbf{V} \mathbf{K}^H \mathbf{K} \mathbf{V}^H = \mathbf{V} \mathbf{V}^H = \mathbf{I}_M$ . It can be observed that a matrix that is orthogonal in the frequency domain is also orthogonal in the time domain.

### 3.3 | Permutation matrix $\mathbf{E}_p$

The matrix  $\mathbf{P}$  can be represented with three block matrices

$$\mathbf{P} = \begin{bmatrix} \mathbf{P}_b \\ \mathbf{P}_m \\ \mathbf{P}_e \end{bmatrix}, \quad (11)$$

where  $\mathbf{P}_b \in \mathbb{C}^{L_b \times M}$ ,  $\mathbf{P}_m \in \mathbb{C}^{(N-L_b-L_c) \times M}$ , and  $\mathbf{P}_e \in \mathbb{C}^{L_c \times M}$ . Copying the  $\mathbf{P}_b$  block matrix and attaching it below  $\mathbf{P}_e$ , and copying the  $\mathbf{P}_e$  block matrix and placing it in front of  $\mathbf{P}_b$  yields an extended OFDM subcarrier matrix

$$\mathbf{Q} = \mathbf{E}_p \mathbf{P} = \begin{bmatrix} \mathbf{P}_e \\ \mathbf{P}_b \\ \mathbf{P}_m \\ \mathbf{P}_e \\ \mathbf{P}_b \end{bmatrix} = \begin{bmatrix} \mathbf{P}_e \\ \mathbf{P} \\ \mathbf{P}_b \end{bmatrix}, \quad (12)$$

where  $\mathbf{Q} \in \mathbb{C}^{(N+L_b+L_c) \times M}$  and  $\mathbf{E}_p$  is a permutation matrix

$$\mathbf{E}_p = \begin{bmatrix} \mathbf{0} & \mathbf{0} & \mathbf{I}_{L_b} \\ \mathbf{0} & \mathbf{I}_N & \mathbf{0} \\ \mathbf{I}_{L_c} & \mathbf{0} & \mathbf{0} \end{bmatrix}, \quad (13)$$

where  $\mathbf{E}_p \in \mathbb{R}^{(L_b+N+L_c) \times (L_b+N+L_c)}$ .

### 3.4 | Weighting matrix $\mathbf{W}$ : Soft transition in the time domain

The weighting matrix gradually increases the magnitudes of both ends of the OFDM symbol and then gradually decreases them. The reason for this is to eliminate the abrupt jump at the beginning and end of the OFDM symbol, which is the reason for the spectrum spread of the OFDM symbol. To remove the jumps, we multiply the weight function equally to each carrier of the OFDM symbol. The weighting function smoothly ramps up and down to limit spectral spreading. Therefore, it is an important function that limits the spectrum of OFDM, and it should be decided according to the specification of the system to be used.

For blocking the OoBE, the spectrum of the input signal must be limited. To do so, all the subcarriers must begin at 0 and end at 0. Multiplying  $\mathbf{Q}$  by the weighting matrix, we have

$$\mathbf{R} = \mathbf{W} \mathbf{Q} = \mathbf{W} \mathbf{E}_p \mathbf{P}, \quad (14)$$

where  $\mathbf{W}$  is a diagonal matrix

$$\mathbf{W} = \text{diag}(\boldsymbol{\kappa}), \quad (15)$$

where  $\boldsymbol{\kappa} = [\kappa_1, \kappa_2, \dots, \kappa_{N+L_b+L_c}]^T$  is a weighting vector.

### 3.5 | Zero insertion to the bandwidth boundaries

The zero insertion at the band boundaries in the frequency domain is performed by filtering in the time domain. The weighted matrix  $\mathbf{R}$  is filtered as

$$\mathbf{G} = \mathbf{R} \otimes_c \mathbf{h}, \quad (16)$$

where  $\mathbf{h} = [h_1, h_2, \dots, h_{r+1}]^T$  is an  $r$ -th-order filter coefficient vector in the time domain,  $\otimes_c$  denotes the convolution of the columns of  $\mathbf{R}$  and the vector  $\mathbf{h}$ , and the size of  $\mathbf{G}$  is  $L \times M$ . Here,  $r$  is set to an even number to simplify the formulas. From Appendix B, the matrix  $\mathbf{G}$  can be expressed in another form as

$$\mathbf{G} = \mathbf{F}_L^H \boldsymbol{\Omega} \mathbf{F}_L \mathbf{E}_r \mathbf{W} \mathbf{E}_p \mathbf{P}, \quad (17)$$

where  $\boldsymbol{\Omega}$  is a diagonal matrix

$$\boldsymbol{\Omega} = \text{diag}(\boldsymbol{\omega}), \quad (18)$$

where  $\boldsymbol{\omega} = [\omega_1, \omega_2, \dots, \omega_L]^T$  is a filtering coefficient vector in the frequency domain.

### 3.6 | Precoder matrix $\mathbf{\Lambda}$

The matrix  $\mathbf{G}$  can be expressed with three block matrices as

$$\mathbf{G} \equiv \begin{bmatrix} \mathbf{G}_h \\ \mathbf{G}_c \\ \mathbf{G}_t \end{bmatrix}. \quad (19)$$

where  $\mathbf{G}_h \in \mathbb{C}^{L_p \times M}$ ,  $\mathbf{G}_c \in \mathbb{C}^{N \times M}$ , and  $\mathbf{G}_t \in \mathbb{C}^{L_s \times M}$ , where  $L_p = \lfloor L_b + r/2 \rfloor$  and  $L_s = \lfloor L_c + r/2 \rfloor$ .

We define an orthogonalization function  $f(\mathbf{G}_c)$  that makes the center matrix  $\mathbf{G}_c$  orthogonal, regardless of the weighting and filtering matrices. The matrix function  $f(\mathbf{G}_c)$  is also multiplied to the head matrix  $\mathbf{G}_h$  and the tail matrix  $\mathbf{G}_t$  to maintain the continuity of the subcarriers.

The orthogonalizing matrix is defined as

$$\mathbf{X} \equiv f(\mathbf{G}_c) = (\mathbf{G}_c^H \mathbf{G}_c)^{-\frac{1}{2}}, \quad (20)$$

where  $\mathbf{X} \in \mathbb{C}^{M \times M}$ . For a matrix  $\mathbf{X}$  to exist, the rank of the matrix  $\mathbf{G}_c$  must be  $M$  so that the rank of  $\mathbf{G}_c^H \mathbf{G}_c$  is  $M$ . The factors influencing the rank of  $\mathbf{G}_c$  are determined by the weighting and zero insertion functions. We can prevent the rank from falling below  $M$ , as it will be mentioned later. As the order of the zero insertion function is sufficient as  $r = 2$ , setting the prefix and suffix length of the weighting function one sample less than the final length while maintaining the length of the center weighting function at  $N$  will never reduce the rank of  $\mathbf{G}_c$ .

A precoder matrix is defined by multiplying the matrix  $\mathbf{G}$  by  $\mathbf{X}$  as.

$$\mathbf{\Lambda} \equiv \mathbf{G} \mathbf{X}, \quad (21)$$

where  $\mathbf{\Lambda} \in \mathbb{C}^{(L_p+N+L_s) \times M}$ .

As  $\mathbf{G}$  is multiplied by  $\mathbf{X}$ , the rows in  $\mathbf{\Lambda}$  become curves without any jumps. The matrix  $\mathbf{\Lambda}$  is represented with three blocks as.

$$\mathbf{\Lambda} \equiv \begin{bmatrix} \mathbf{\Lambda}_h \\ \mathbf{\Lambda}_c \\ \mathbf{\Lambda}_t \end{bmatrix} = \begin{bmatrix} \mathbf{G}_h \\ \mathbf{G}_c \\ \mathbf{G}_t \end{bmatrix} \mathbf{X}. \quad (22)$$

where the block matrices  $\mathbf{\Lambda}_h \in \mathbb{C}^{L_p \times M}$ ,  $\mathbf{\Lambda}_c \in \mathbb{C}^{N \times M}$ , and  $\mathbf{\Lambda}_t \in \mathbb{C}^{L_s \times M}$  are head, center, and tail matrices, respectively. The center matrix is

$$\mathbf{\Lambda}_c = \mathbf{G}_c \mathbf{X} = \mathbf{G}_c (\mathbf{G}_c^H \mathbf{G}_c)^{-\frac{1}{2}}, \quad (23)$$

which is orthogonal because it has the same form as (8). In other words, the center matrix in the precoder, which is responsible for transmitting information, is orthogonal. In a method of transmitting information through an orthogonal matrix, when received through a multipath fading channel, orthogonality between subcarriers may be impaired, thereby preventing orthogonal reception. In such a case, each subcarrier for transmitting each data symbol is formed from many OFDM subcarriers. When received through a multipath fading channel, orthogonality is impaired between the subcarriers, resulting in a decrease in reception performance. In other words,  $\mathbf{\Lambda}_c^H \mathbf{\Lambda}_c = \mathbf{I}$  cannot be guaranteed. Consequently, each column vector of the orthogonal matrix that transmits the information must be composed of a single frequency to realize ideal transmission. However, as will be discussed in the next subsection, as  $\mathbf{\Lambda}_c$  is very similar to  $\mathbf{P}$  formed with a single frequency, the symbols transmitted by the proposed scheme are robust to the effects of the multipath fading channel.

### 3.7 | Approximated precoder

In the previous section, we mentioned that, in the ideal transmission method, a subcarrier for transmitting information is formed with a single frequency. In this section, the proposed scheme shows that the center matrix responsible for information transmission is very close to the matrix  $\mathbf{P}$  used in the OFDM system. As it is difficult to know exactly the role played by the precoder matrix given by (21), we analyze the inner blocks in more detail. From Appendix C, the center matrix can be approximated as.

$$\mathbf{G}_c \approx \mathbf{F}_N^H \mathbf{\Omega} \mathbf{F}_N \mathbf{W}_c \mathbf{P} \quad (24)$$

and the center matrix  $\mathbf{\Lambda}_c$  can be represented approximately as

$$\mathbf{\Lambda}_c \approx \mathbf{P}, \quad (25)$$

which shows that the center matrix of the precoder is close to the matrix  $\mathbf{P}$  in which the subcarriers are formed at a single frequency in OFDM. We define an approximated precoder as

$$\mathbf{\Lambda}_{\text{appx}} = \begin{bmatrix} \mathbf{\Lambda}_h \\ \mathbf{P} \\ \mathbf{\Lambda}_t \end{bmatrix}. \quad (26)$$

It can be observed that the proposed approximated precoding scheme is similar to CP-OFDM.

### 3.8 | Pilot insertion

Pilot insertion in the transmitter is essential for channel estimation. Therefore, the new transmission technique needs to be checked not only for spectral efficiency but also for the ability to transmit the pilot securely. The interference between subcarriers in the frequency domain for pilot transmission is examined.

From (25), the center matrix  $\mathbf{\Lambda}_c$  can be represented in the frequency domain as.

$$\mathbf{\Phi}_c = \mathbf{F}_N \mathbf{\Lambda}_c \approx \mathbf{F}_N \mathbf{P} = \mathbf{J}, \quad (27)$$

which is the mapping matrix. As  $\mathbf{\Phi}_c$  is close to  $\mathbf{J}$ , the interferences between subcarriers in  $\mathbf{\Phi}_c$  can be ignored. Therefore, the pilots can be transmitted on arbitrary subcarriers, and various pilot insertion methods used in CP-OFDM can be utilized without any change.

## 4 | GENERATION OF PRECODER MATRIX WITH A SHORT PACKET/ SYMBOL

This section shows the process of generating a precoder matrix according to the IEEE 802.11a standard that specifies the OFDM symbol in the context of a detailed description of the proposed scheme. In the specification, a short OFDM symbol consists of a CP with  $L_{cp} = 16$  samples and an IFFT symbol with  $N = 64$  samples, and has a total length of  $L = 80$  samples. There is also a zero-frequency subcarrier and  $M = 52$  occupied subcarriers. According to the specification, a precoder matrix with parameters  $r = 2$ ,  $L_p = L_s = 8$ , and  $L_{GI} = 16$  is generated with the same occupied carriers and OFDM symbol length as the specified OFDM.

### 4.1 | Generation of a precoder matrix

This section shows the process of generating a precoder with the small OFDM symbols specified in IEEE 802.11a in a spectrally efficient scheme. The result is to obtain an orthogonal matrix while maintaining the original center matrix and to change the prefix and suffix parts with the obtained matrix. As the center matrix approximately returns to the mapping matrix, the newly generated prefix and suffix should have spectral efficiency.

Figure 3A shows a part of a matrix  $\mathbf{P} \in \mathbb{C}^{(64 \times 52)}$  transforming the frequency-domain subcarriers into the time domain, where only 16 of the 64 subcarriers are shown here for clarity of illustration. In the figure, the real and imaginary parts are symmetric and skew-symmetric, respectively, from the center. It can be observed that the subcarriers in the real part have a sudden jump at the beginning and the end, which is the main factor causing spreading of the spectrum.

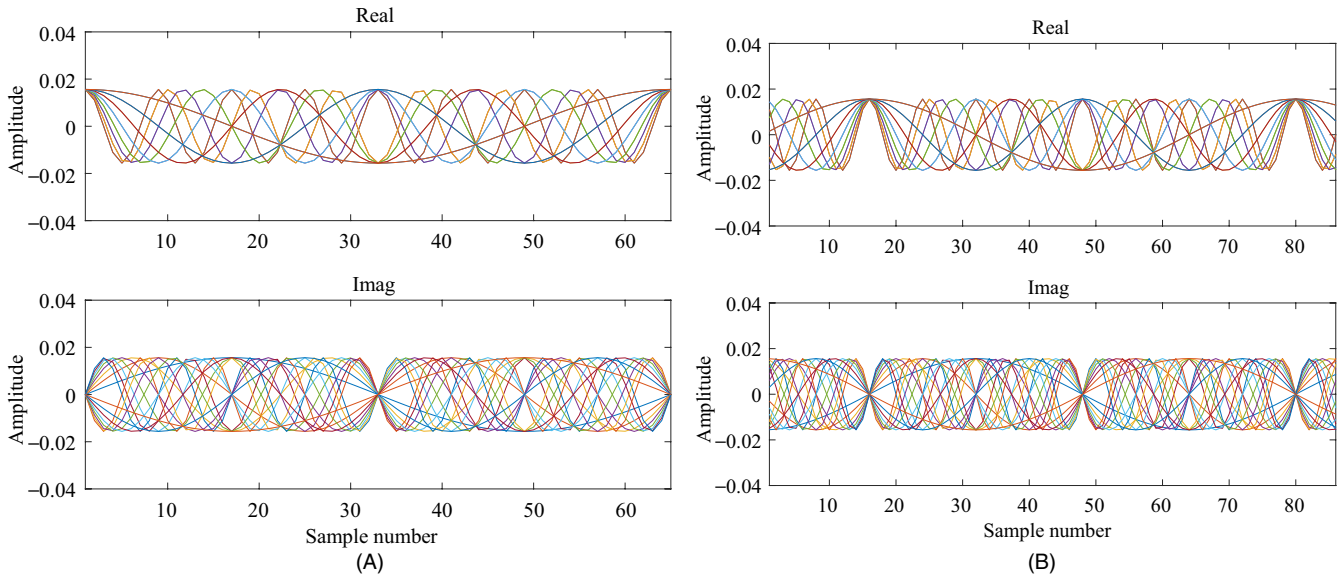
Figure 3B shows the result of copying  $L_e (= 7)$  samples of the front part of the IFFT symbol, attaching it after the IFFT symbol, and copying  $L_b + L_{cp} (7 + 8 = 15)$  samples after the IFFT symbol and placing them in front of the IFFT symbol. In this process, the original center part remains intact.

The window function is required to be symmetric and must have a value of 0 at both ends. As it is important to suppress the spread of the spectrum of the signal, the window function is preferably a smooth curve without jumps. We define a weighting function as.

$$\kappa_h(n) = x(n), \quad 0 \leq n \leq L_b - 1, \quad (28)$$

$$\kappa_c(n) = 1, \quad 0 \leq n < N - 1, \quad (29)$$

$$\kappa_t(n) = x(L_b - 1 + n), \quad 0 \leq n < L_e - 1, \quad (30)$$

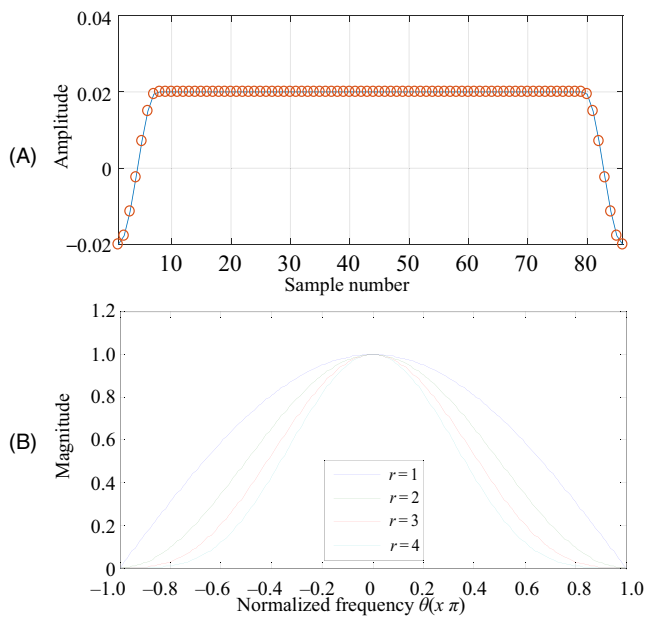


**FIGURE 3** (A) Subcarriers in the time domain with  $\beta=11, M=16, N=64$ . (B) Cyclic extension with  $r=2, \beta=11, L_b=L_e=7, L_{cp}=8, M=16, N=64$

where

$$x(s) = \frac{1}{2} \left( 1 - \cos \frac{2\pi s}{L_b + L_e - 2} \right). \quad (31)$$

Figure 4A is an example of a window function with a weighting vector  $\mathbf{\kappa}$  with  $L_b = L_e = 7, L_{cp} = 8$ , and  $N = 64$ , which can be used for a short OFDM symbol with 72 samples. The center portion of the function is maintained flat, whereas the front and back portions of the function are gradually increased or gradually decreased so that the entire curve becomes smooth



**FIGURE 4** (A) Weighting vector  $\zeta$  with  $L_b = L_e = 7, L_{cp} = 8$  surrounded by the Hanning window, where  $o$  denotes a sample point. (B) Frequency responses of the binomial filters

The filtering function makes the magnitudes zero at the frequency band boundaries, where the interference power is blocked from flowing into the neighboring channel. As a filter function satisfying the condition, a binomial filter.

$$h(z) = \frac{1}{2^r} (1 + z^{-1})^r, \quad (32)$$

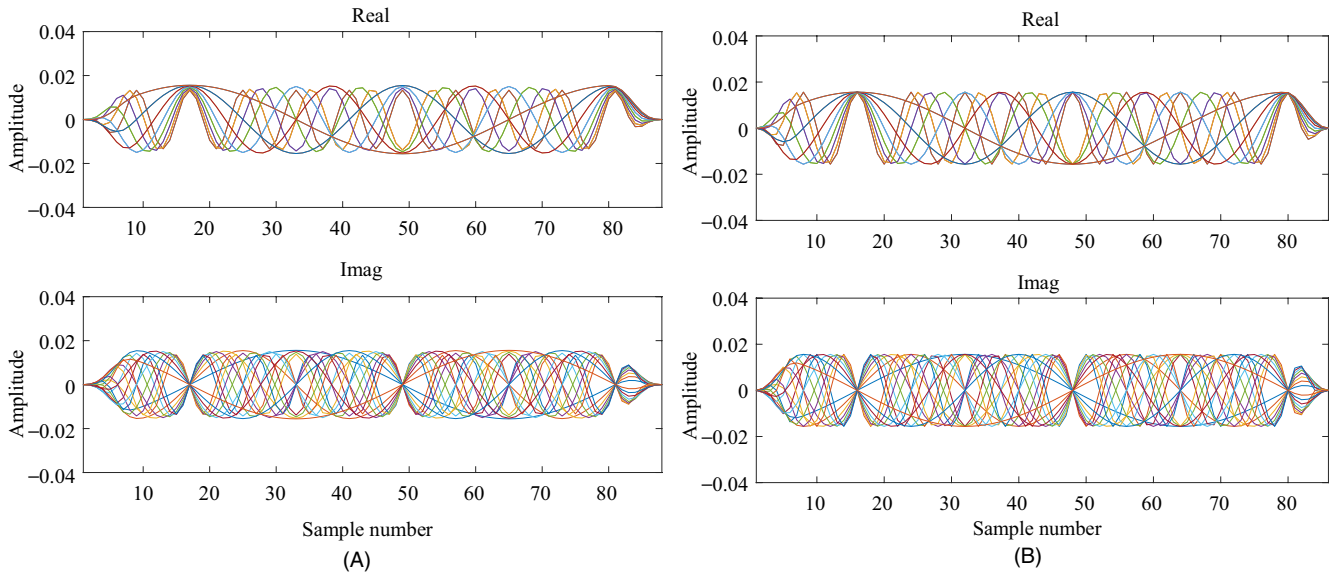
where  $r$  is the filter order, is considered. The filtering vector  $\mathbf{h}$  in the time domain is composed of the coefficients of  $\omega(\theta)$  as

$$\omega(\theta) = h(z) \Big|_{z=e^{j\theta}} = e^{-\frac{jr\theta}{2}} \cos^r \frac{\theta}{2}, \quad (33)$$

The filtering vector  $\omega$  in the frequency domain can be obtained by sampling the function  $\omega(\theta)$ .

Figure 4B shows the frequency responses of the filters according to the orders. The feature of this filter is that it can be implemented with a short filter with a small order  $r$  from the filter function given by (28), and it blocks the OoBE because  $\omega(\pm\pi) = 0$ .

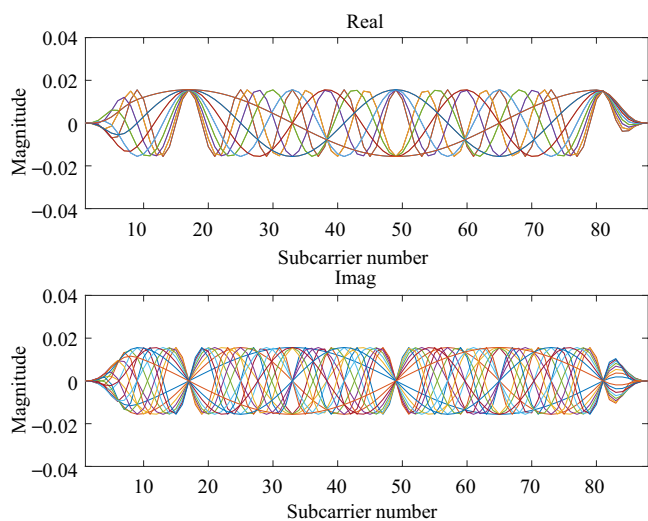
Figure 5 shows the waveform shaped by using window and filtering functions. Figure 5A shows the result when the input matrix is multiplied by the window matrix  $\mathbf{W}$ , where the amplitudes of the subcarriers gradually increase and decrease in the head and tail, respectively, and the center part remains constant. Figure 5B shows the result of filtering the column of the input matrix when the order  $r = 2$ . It can be observed that the subcarriers are much smoother than in Figure 5A. To match the length with that specified in IEEE 802.11a, the prefix and suffix lengths of the input matrix are set to 7. If filtering by a filter of order 2 is performed, the filtering result is increased by two samples.



**FIGURE 5** (A) Windowed subcarriers with  $\beta = 11, L_b = L_c = 7, L_{cp} = 8, M = 16, N = 64$ . (B) Filtered subcarriers with  $r = 2, L_b = L_c = 8, L_{cp} = 8, M = 16, N = 64$

Figure 6 shows the subcarriers, which are the columns of the final precoder matrix obtained through the orthogonalization process in (17). Compared with Figure 5B, the overall shape is similar, but the beginning and end of the center curves are clear because the curves of all the columns of the generated precoder matrix intersect at the beginning and end of the center matrix. Consequently, the center part returns to the original part of Figure 3A, and the head and tail parts of Figure 6 are transformed into the waveforms with spectrum that are defined through windowing, zero insertion, and orthogonalization.

Thus far, we have demonstrated the process of generating a precoder matrix with the OFDM symbol according to IEEE 802.11a. If a spectral prefix and suffix are attached to a legacy OFDM symbol, transmission efficiency may be reduced.

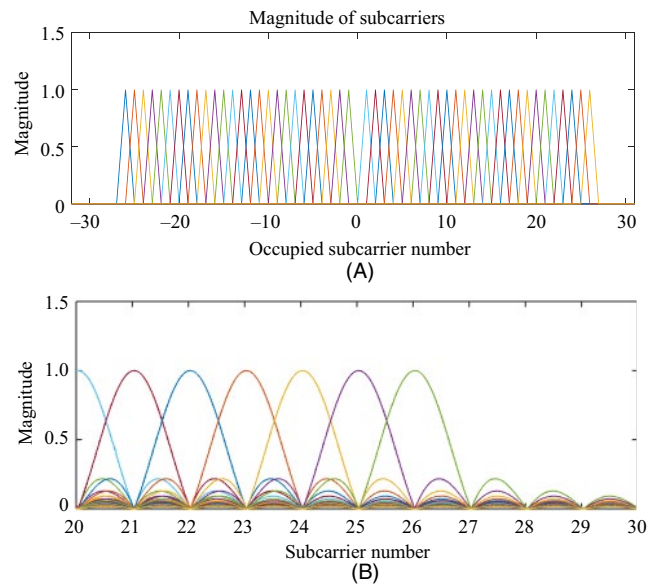


**FIGURE 6** Subcarriers of the precoder generated with  $r = 2, \beta = 11, L_p = L_s = 8, L_{cp} = 8, M = 16, N = 64$

To solve such a problem, IEEE 802.11g requires that a prefix be used in a CP, and a suffix transmits the overlapping prefix of the successive OFDM symbol. The proposed method also shows an example of precoder occurrence in subsection 4.1. Therefore, the proposed spectrally encapsulated (SE)-OFDM does not degrade the throughput of legacy OFDM.

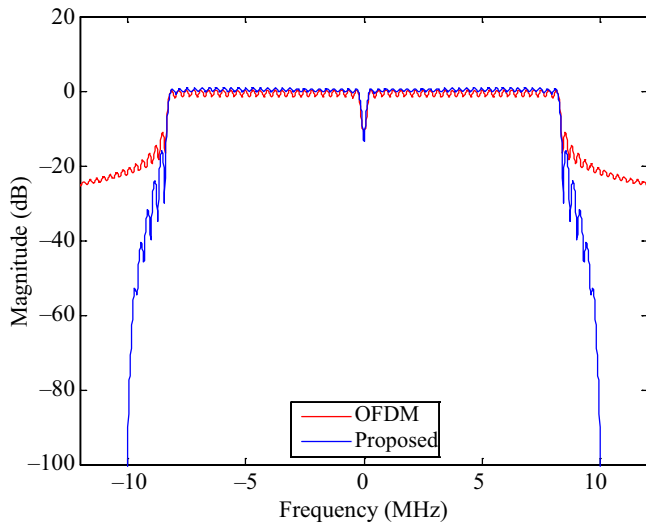
### 4.2 | Frequency response

Figure 7A shows subcarriers that are the columns of the center matrix  $\Lambda_c$  in the frequency domain, where the size of the IFFT



**FIGURE 7** Frequency domain representation of the center matrix  $\Lambda_c$  with  $r = 2, \beta = 11, L_p = L_s = 4, L_{cp} = 8, M = 52, N = 64$ . (A) Subcarriers in the frequency domain. (B) Interpolated figure of (A)





**FIGURE 8** Frequency responses of legacy CP-OFDM and the proposed scheme with  $r = 2, \beta = 11, L_p = L_s = 8, L_{cp} = 8, L_{GI} = 16, M = 52, N = 64$

symbol is 64 according to the IEEE 802.11a standard and 52 subcarriers are occupied. The groups on the left and right of the center represent subcarriers with positive and negative frequencies, respectively, which are distributed evenly in the entire band without affecting one another. In particular, it can be observed that the 26th subcarrier, which is the boundary of the band in Figure 7B, maintains orthogonality without being influenced by the generation process of the precoder matrix. In the proposed scheme, the subcarriers in the center part that transmit the data symbols have orthogonality as in CP-OFDM, but the subcarriers of the entire OFDM symbol are nonorthogonal and restrict the spectrum to suppress the OoBE.

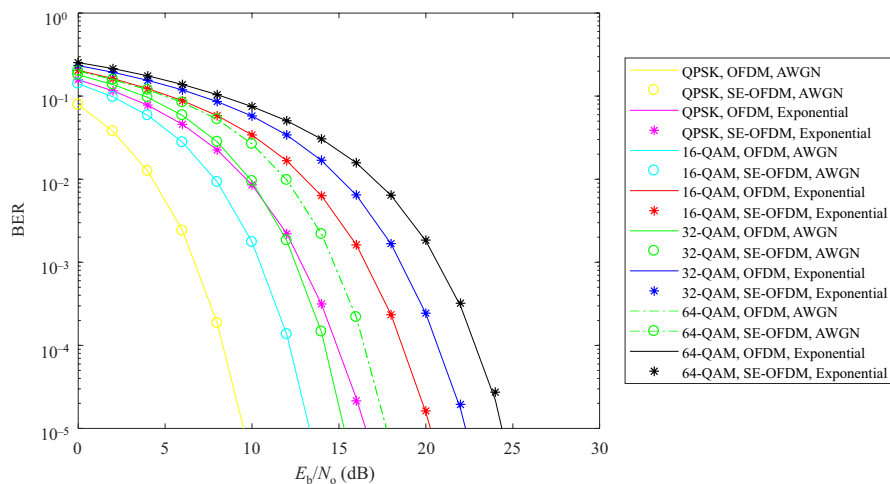
Figure 8 shows the frequency response characteristic of the approximated precoder when the precoder is designed according to the IEEE 802.11a standard. The frequency response characteristics of CP-OFDM and the proposed scheme

in the passband are identical, but the size of the CP-OFDM gradually decreases while passing the passband, whereas that of the proposed scheme is drastically reduced and the stopband edge reaches the channel band boundaries. One of the advantages of the proposed scheme is that the stopband edge does not cross the channel band boundary because the signal powers at the frequency boundaries are zero. In the figure, it is confirmed that the precoded signal obtained via the proposed scheme does not exceed the channel boundaries of  $\pm 10$  (MHzGI). The spectral characteristic of the proposed scheme is superior to that of [21], which does not have spectral cliffs at band boundaries.

## 5 | BER PERFORMANCE

As OFDM has ideal BER performance except for the issue of OoBE; the performance of the proposed SE-OFDM scheme is compared with that of CP-OFDM. The BER performance is obtained through an AWGN channel and a multipath fading channel, which is modeled as an exponentially delayed channel,  $h(k) = C \cdot 10^{-k/10}, k = 0, 1, \dots, 7$  [15], where  $C$  is the power normalizing factor.

The performance of the proposed SE-OFDM is consistent with that of ideal CP-OFDM; hence, the orthogonality of the IFFT symbol among the precoded OFDM symbols is not damaged in the precoding process. Figure 9 shows the performances of OFDM and the proposed scheme when data are transmitted through AWGN and exponentially delayed channels. The BER performance of the proposed scheme is evaluated, where the data symbols of quadrature phase shift keying (QPSK), 16-QAM, 32-QAM, and 64-QAM are received through two types of channels. The performance of the proposed SE-OFDM scheme through an AWGN channel is consistent with that of CP-OFDM, which indicates that the IFFT symbol in the precoded signal obtained via the proposed scheme is not changed.



**FIGURE 9** BER performances of CP-OFDM and the proposed SE-OFDM scheme with  $r = 2, \beta = 11, L_p = L_s = 8, L_{GI} = 16, M = 52, N = 64$

TABLE 1 Scheme-specific characteristics

Schemes	Self-interference	Equalizer	Spectral efficiency	Autocorrelation	BER
OFDM	NE	NR	Low	High	Ideal
FBMC	EX	RQ	Very high	High	Good
F-OFDM	EX	RQ	High	Medium	Good
E-GFDM [21]	EX	RQ	Medium high	High	Good
SP-OFDM [4]	NE	NR	High	High	Good
OP [7]	NE	NR	High	High	Good
N-OFDM [8]	NE	NR	High	High	Good
GSS-OFDM [13]	NE	NR	High	High	Ideal
Proposed SE-OFDM	NE	NR	Nearly perfect	High	Nearly ideal

Abbreviations: NE, Nonexistence; EX, Existence; NR, Not required; RQ, Required; Nearly Perfect indicates not mathematically perfect, but engineering perfect. Nearly Ideal indicates not mathematically ideal, but engineering ideal.

The performance of the proposed SE-OFDM scheme through a multipath fading channel is consistent with that of CP-OFDM, which indicates that the CP-OFDM symbol in the changed signal obtained via the orthogonalizing matrix is negligibly changed. Therefore, it is confirmed that the performances of CP-OFDM and the proposed SE-OFDM scheme are consistent for the four modulation schemes and over the two channel environments. The F-OFDM shows that the receiver has the same characteristics as CP-OFDM through equalization. However, the proposed scheme does not require any decoder or equalizer at the receiver owing to the transmission scheme, and thus can be implemented more simply than the F-OFDM. The E-GFDM has also been developed to eliminate self-interference, improving the BER performance to the same level as that of CP-OFDM. However, this method is inferior to the proposed SE-OFDM method because the spectral characteristics are not recommended for evaluation based on the BER performance alone [21]. Table 1 summarizes the issues discussed so far.

## 6 | CONCLUSION

In this study, we proposed the SE-OFDM precoding scheme to block the OoBE of OFDM systems. This method can maintain transmission efficiency by encapsulating existing OFDM without using internal information such as CC or external information such as CSI. The demodulation scheme of SE-OFDM can be performed in the same way as that of legacy OFDM as it does not change the IFFT symbol carrying data in the precoding process. It is also meaningful that the problem of spectrum spreading is solved without impairing the advantage of the CP-OFDM. This fact is confirmed by simulating the OFDM symbol defined in IEEE 802.11a in actual use. To verify the practicality of the proposed scheme, pilot insertion methods were investigated for channel estimation. The mapping matrix used in CP-OFDM is transformed into the precoder matrix via IDFT, permutation, weighting, zero insertion, and orthogonalization. It was confirmed from the frequency

response characteristics that the generated precoder could suppress OoBE effectively. The BER performance of the proposed scheme is obtained through two types of channels and compared with that of CP-OFDM, which shows an ideal performance. By confirming that the performance of the proposed scheme is consistent with that of CP-OFDM, the proposed scheme can be considered to have an optimal design. The proposed scheme is expected to be useful for future wireless local area networks and Internet of things, which require small low-power systems.

## ACKNOWLEDGMENTS

The authors wish to thank Dr. Lim Jong Soo at ETRI for the helpful discussions and the anonymous reviewers for their valuable comments.

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## APPENDIX A

Orthogonal matrix  $\mathbf{P}$ 

$$\begin{aligned}
\mathbf{P} &= \mathbf{U}\mathbf{\Sigma}\mathbf{V}^H \left( (\mathbf{U}\mathbf{\Sigma}\mathbf{V}^H)^H (\mathbf{U}\mathbf{\Sigma}\mathbf{V}^H) \right)^{-\frac{1}{2}} \\
&= \mathbf{U}\mathbf{\Sigma}\mathbf{V}^H (\mathbf{V}\mathbf{\Sigma}^H \mathbf{U}^H \mathbf{U}\mathbf{\Sigma}\mathbf{V}^H)^{-\frac{1}{2}} \\
&= \mathbf{U}\mathbf{\Sigma}\mathbf{V}^H (\mathbf{V}\mathbf{\Sigma}^H \mathbf{\Sigma}\mathbf{V}^H)^{-\frac{1}{2}} \\
&= \mathbf{U}\mathbf{\Sigma}\mathbf{V}^H \left( \mathbf{V} \begin{bmatrix} \mathbf{S} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \mathbf{S} \\ \mathbf{0} \end{bmatrix} \mathbf{V}^H \right)^{-\frac{1}{2}} \\
&= \mathbf{U}\mathbf{\Sigma}\mathbf{V}^H (\mathbf{V}\mathbf{S}^2\mathbf{V}^H)^{-\frac{1}{2}} \\
&= \mathbf{U}\mathbf{\Sigma}\mathbf{V}^H \left( (\mathbf{V}\mathbf{S}\mathbf{V}^H)^2 \right)^{-\frac{1}{2}} \\
&= \mathbf{U} \begin{bmatrix} \mathbf{S} \\ \mathbf{0} \end{bmatrix} \mathbf{V}^H \mathbf{V}\mathbf{S}^{-1}\mathbf{V}^H \\
&= \mathbf{U} \begin{bmatrix} \mathbf{I}_M \\ \mathbf{0} \end{bmatrix} \mathbf{V}^H \\
&= \mathbf{U}\mathbf{K}\mathbf{V}^H,
\end{aligned} \tag{A1}$$

where  $(\mathbf{V}\mathbf{S}\mathbf{V}^H)^{-1} = (\mathbf{V}^H)^{-1}\mathbf{S}^{-1}\mathbf{V}^{-1} = \mathbf{V}\mathbf{S}^{-1}\mathbf{V}^H$  from the inverse matrix property and  $\mathbf{V}^{-1} = \mathbf{V}^H$  are used, and

$$\mathbf{K} = \begin{bmatrix} \mathbf{I}_M \\ \mathbf{0} \end{bmatrix}. \tag{A2}$$

Especially, when  $M = N$ , the diagonal matrix becomes

$$\mathbf{K} = \mathbf{I}_N \tag{A3}$$

and

$$\mathbf{P} = \mathbf{U}\mathbf{V}^H. \tag{A4}$$

## APPENDIX B

Representation of matrix  $\mathbf{G}$  as a product of matrices

Attaching  $r$  zeros to each column of matrix  $\mathbf{R}$ , the matrix is expressed as

$$\mathbf{B} = \mathbf{E}_r \mathbf{R}, \tag{B1}$$

where

$$\mathbf{E}_r = \begin{bmatrix} \mathbf{I}_p \\ \mathbf{0}_{(r \times N)} \end{bmatrix}. \tag{B2}$$

The matrix  $\mathbf{B}$  is transformed into the frequency domain as

$$\mathbf{K} = \mathbf{F}_L \mathbf{B} = \mathbf{F}_L \mathbf{E}_r \mathbf{R}, \tag{B3}$$

where  $L = N + L_p + L_s$ . The filter matrix  $\mathbf{\Omega}$  is multiplied to perform filtering in the frequency domain as

$$\mathbf{\Phi} = \mathbf{\Omega} \mathbf{F}_L \mathbf{E}_r \mathbf{R}. \tag{B4}$$

Upon converting this matrix back into the time domain, it becomes

$$\mathbf{G} = \mathbf{F}_L^H \mathbf{\Omega} \mathbf{F}_L \mathbf{E}_r \mathbf{R}. \tag{B5}$$

Substituting (14) into (B5), we have

$$\mathbf{G} = \mathbf{F}_L^H \mathbf{\Omega} \mathbf{F}_L \mathbf{E}_r \mathbf{W}_p \mathbf{P}. \tag{B6}$$

## APPENDIX C

Center matrix,  $\Lambda_c$ 

We consider the center matrix in  $\mathbf{G}$  as

$$\mathbf{G}_c = \mathbf{R}_c \otimes_c \mathbf{h}. \tag{C1}$$

As the center matrix of  $\mathbf{E}_p$  is  $\mathbf{I}_N$ , the center matrix in  $\mathbf{R}$  can be written as

$$\mathbf{R}_c = (\mathbf{W}_p \mathbf{P})_c = \mathbf{W}_c \mathbf{P}. \tag{C2}$$

Substituting (C2) into (C1), the center matrix can be written as

$$\mathbf{G}_c = (\mathbf{W}_c \mathbf{P}) \otimes_c \mathbf{h}. \tag{C3}$$

Practically, as the prefix and suffix are sufficiently smaller than the IFFT symbol, the approximated matrix of  $\mathbf{G}_c$  can be represented by substituting  $L$  with  $N$  as

$$\mathbf{G}_c \approx \mathbf{M} = \mathbf{F}_N^H \mathbf{\Omega} \mathbf{F}_N \mathbf{W}_c \mathbf{P}. \tag{C4}$$

The matrices  $\mathbf{\Omega}$  and  $\mathbf{W}_c$  are represented in SVD forms as

$$\mathbf{\Omega} = \mathbf{U}_\Omega \mathbf{\Sigma}_\Omega \mathbf{V}_\Omega^H, \tag{C5}$$

$$\mathbf{W}_c = \mathbf{U}_{W_c} \mathbf{\Sigma}_{W_c} \mathbf{V}_{W_c}^H, \tag{C6}$$

where  $\mathbf{U}_\Omega$ ,  $\mathbf{U}_{W_c}$ ,  $\mathbf{V}_\Omega$ , and  $\mathbf{V}_{W_c}$  are unitary, and  $\mathbf{\Sigma}_\Omega$  and  $\mathbf{\Sigma}_{W_c}$  are diagonal.

As the matrices  $\mathbf{F}_N$  and  $\mathbf{P}$  are all unitary, they cannot contribute to the eigenvalues of  $\mathbf{M}$ . The matrix  $\mathbf{M}$  can be decomposed as

$$\mathbf{M} = \mathbf{U}_M f(\boldsymbol{\Sigma}_\Omega, \boldsymbol{\Sigma}_{\mathbf{W}_c}) \mathbf{V}_M^H, \quad (\text{C7})$$

where  $\mathbf{U}_M$  and  $\mathbf{V}_M^H$  are unitary, and  $f(\boldsymbol{\Sigma}_\Omega, \boldsymbol{\Sigma}_{\mathbf{W}_c})$  is the matrix function with two diagonal matrices  $\boldsymbol{\Sigma}_\Omega$  and  $\boldsymbol{\Sigma}_{\mathbf{W}_c}$ , and can be expressed as

$$f(\boldsymbol{\Sigma}_\Omega, \boldsymbol{\Sigma}_{\mathbf{W}_c}) = \begin{bmatrix} \boldsymbol{\Gamma} \\ \mathbf{0}_{((N-M) \times M)} \end{bmatrix}, \quad (\text{C8})$$

where  $\boldsymbol{\Gamma} \in \mathbb{R}^{(M \times M)} = \text{diag}(\gamma_1, \gamma_2, \dots, \gamma_M)$  is a diagonal matrix with  $M$  eigenvalues.

Based on the same procedure as that in Appendix A, orthogonalizing the matrix  $\mathbf{M}$  yields

$$\mathbf{M}^\perp = \mathbf{U}_M \mathbf{K} \mathbf{V}_M^H. \quad (\text{C9})$$

From this result, it can be observed that  $\mathbf{M}^\perp$  is a constant orthogonal matrix regardless of the matrices  $\boldsymbol{\Omega}$  and  $\mathbf{W}_c$ . To obtain the center matrix, by substituting  $\boldsymbol{\Omega}$  and  $\mathbf{W}_c$  with the identity matrix  $\mathbf{I}_N$ , we have

$$\begin{aligned} \boldsymbol{\Lambda}_c &\approx \mathbf{M}^\perp \Big|_{\mathbf{W}_c = \mathbf{I}_N} \\ &= \mathbf{F}_N^H \boldsymbol{\Omega} \mathbf{F}_N \mathbf{W}_c \mathbf{P} \left[ (\mathbf{F}_N^H \boldsymbol{\Omega} \mathbf{F}_N \mathbf{W}_c \mathbf{P})^H \mathbf{F}_N^H \boldsymbol{\Omega} \mathbf{F}_N \mathbf{W}_c \mathbf{P} \right]^{-\frac{1}{2}} \Big|_{\mathbf{W}_c = \mathbf{I}_N} \\ &= \mathbf{F}_N^H \mathbf{I}_N \mathbf{F}_N \mathbf{I}_N \mathbf{P} \left[ (\mathbf{F}_N^H \mathbf{I}_N \mathbf{F}_N \mathbf{I}_N \mathbf{P})^H \mathbf{F}_N^H \mathbf{I}_N \mathbf{F}_N \mathbf{I}_N \mathbf{P} \right]^{-\frac{1}{2}} \quad (\text{C10}) \\ &= \mathbf{F}_N^H \mathbf{F}_N \mathbf{P} \left[ (\mathbf{F}_N^H \mathbf{F}_N \mathbf{P})^H \mathbf{F}_N^H \mathbf{F}_N \mathbf{P} \right]^{-\frac{1}{2}} \\ &= \mathbf{P} (\mathbf{P}^H \mathbf{P})^{-\frac{1}{2}} \\ &= \mathbf{P}. \end{aligned}$$